

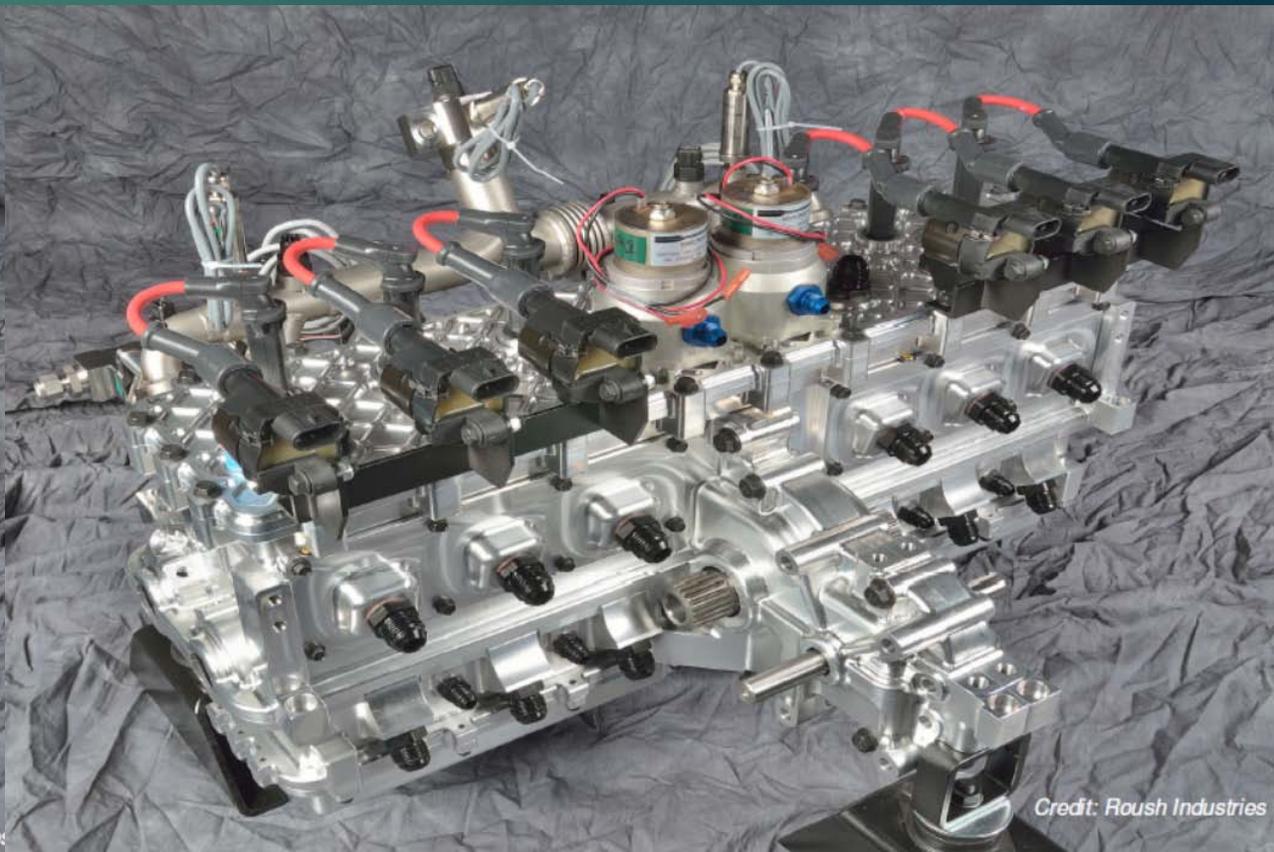


ICESIP: Internal Combustion Engine Solar Independent Propulsion

**for Lunar Polar
Exploration Rovers (LPERs)**

The very idea is not crazy:

1930's-inspired flathead for Centaur 3rd stage invented by United Launch Alliance (ULA)



Why ICESIP?

#1 Reason:

Need for extended operations within permanently shaded regions (PSRs) of Moon

2. Nukes are super-expensive

3. The interesting craters lack solar energy

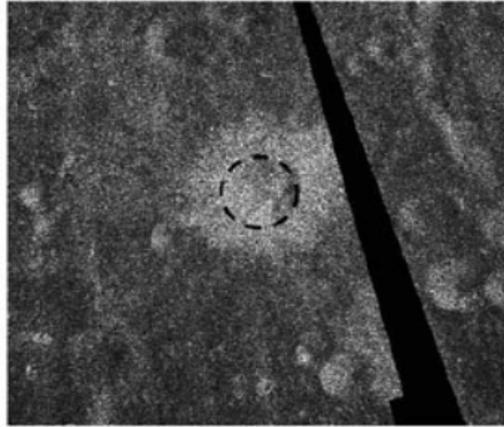
What are the high value targets (HVTs)?

A: the anomalous craters...

Main L



S1



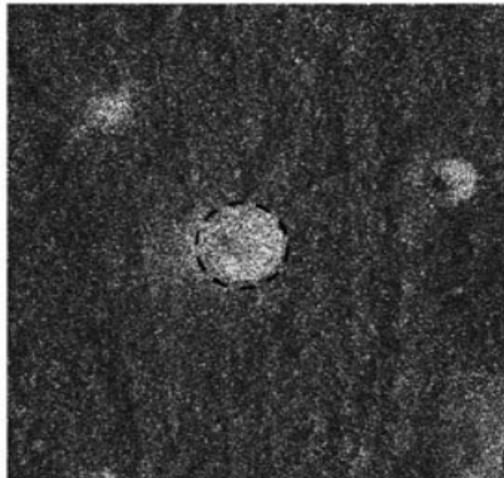
CPR



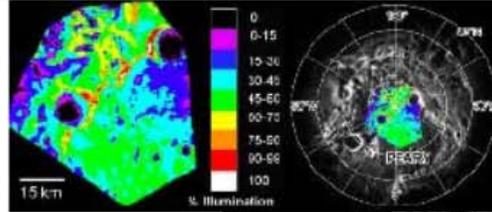
Rozhdestvensky N



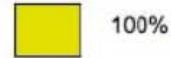
S1



CPR



Illumination (summer)



100%

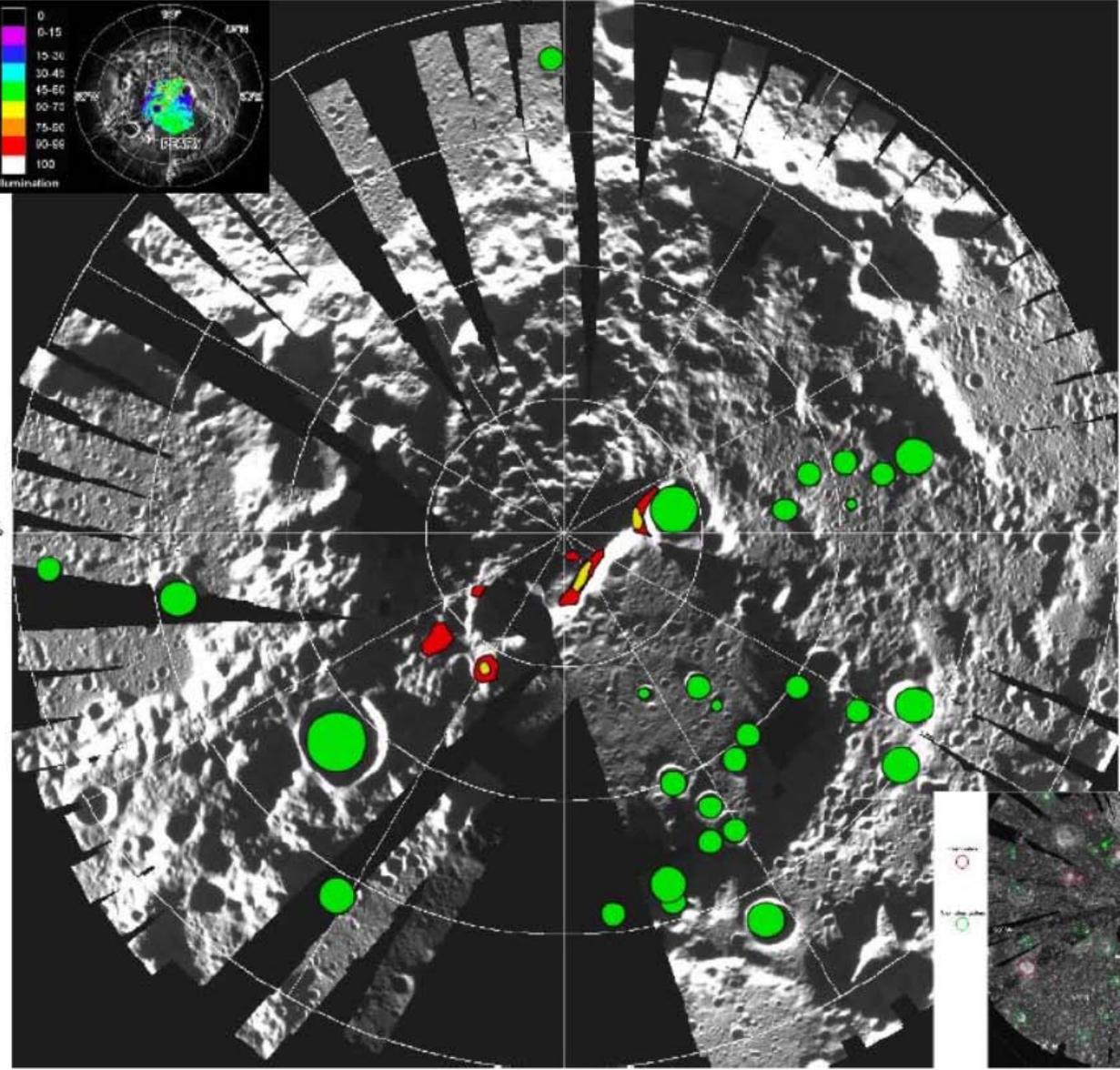


90-100%



High CPR crater fill (ice)

10 km

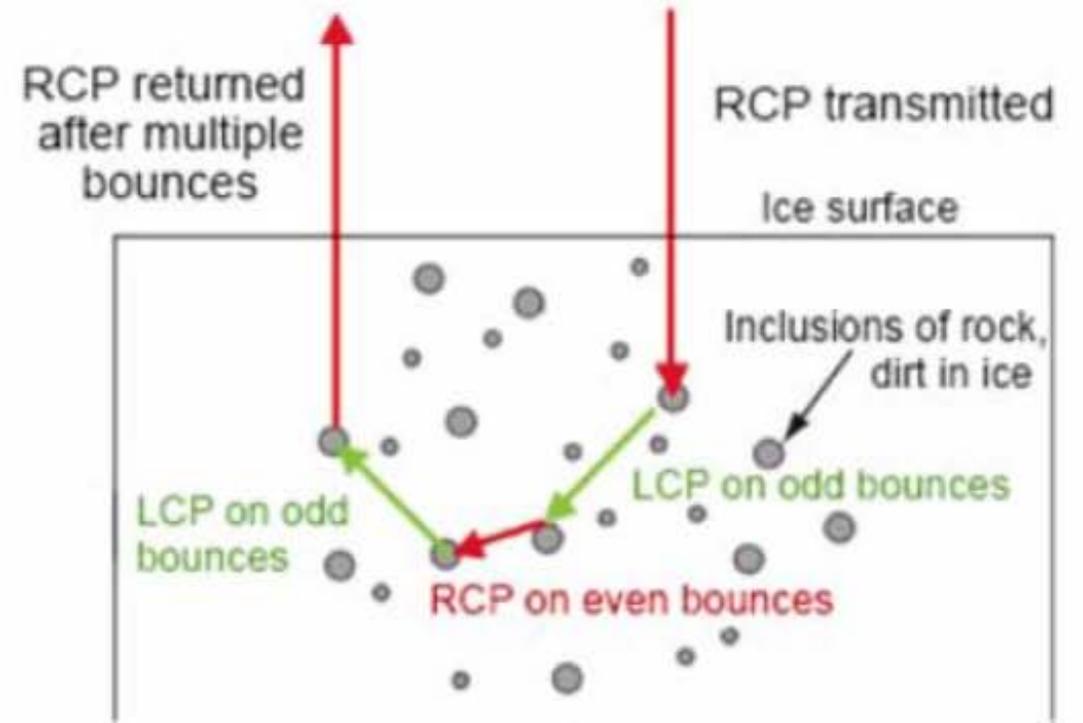
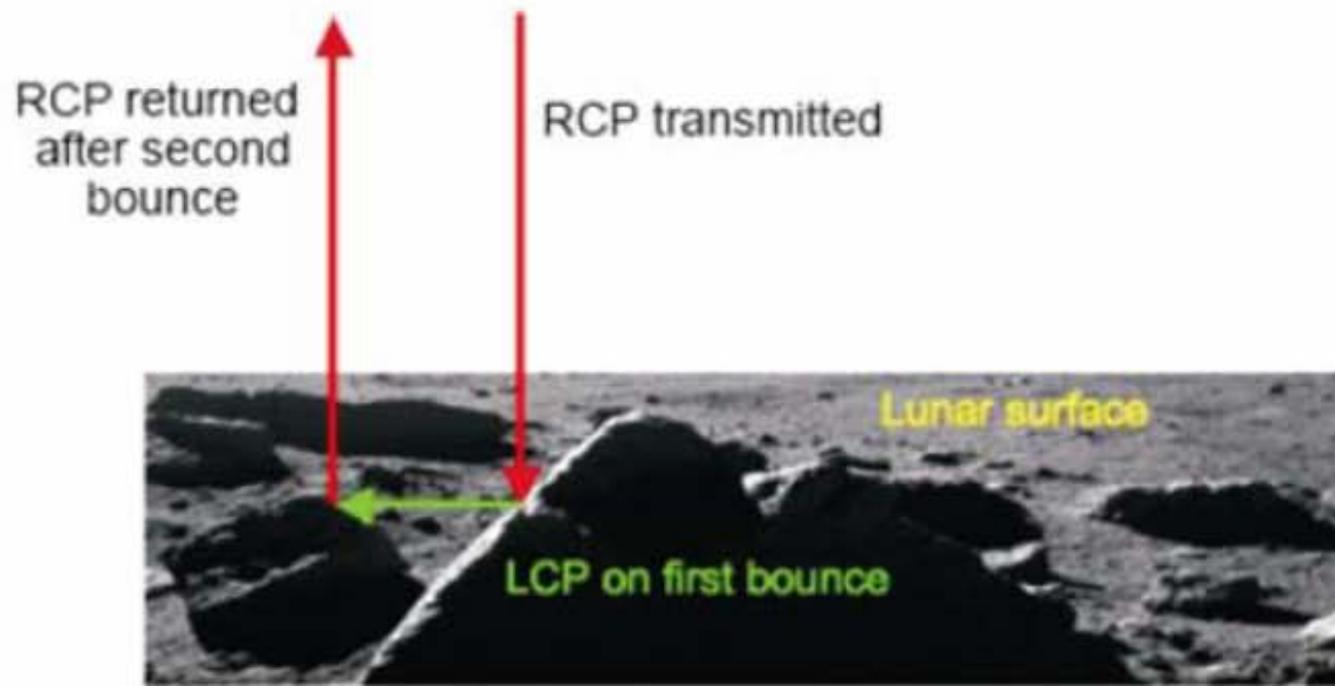


Circular Polarization Ratio (CPR)

- ratio of same-sense to opposite sense circular polarization
- thought to mark “relatively pure” H₂O ice

High CPR caused by surface roughness/scattering

High CPR caused by ice/volume scattering



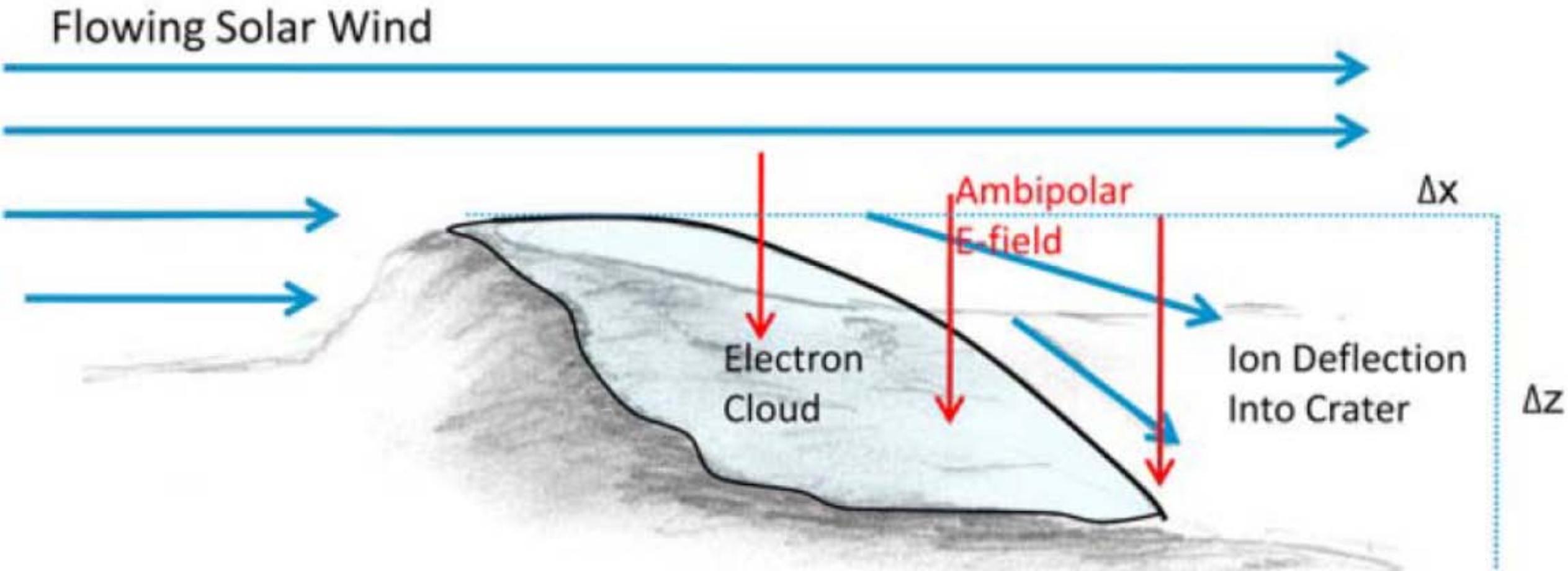
Properties of anomalous craters

1. Extra cold temperatures ($\sim 30^{\circ}\text{K}$)
2. Would have higher H_2O content
3. Ice of unknown texture or density
4. Small (< 20 km) craters within craters
5. Craters tend to be steep sided ($\sim 30^{\circ}$)
6. Zones with low electrostatic activity
7. Possibility of electrostatic placer deposits

6. Effect of solar wind on lunar ice

H⁺ ions will cause erosion of lunar ice

Small craters within craters avoid this effect

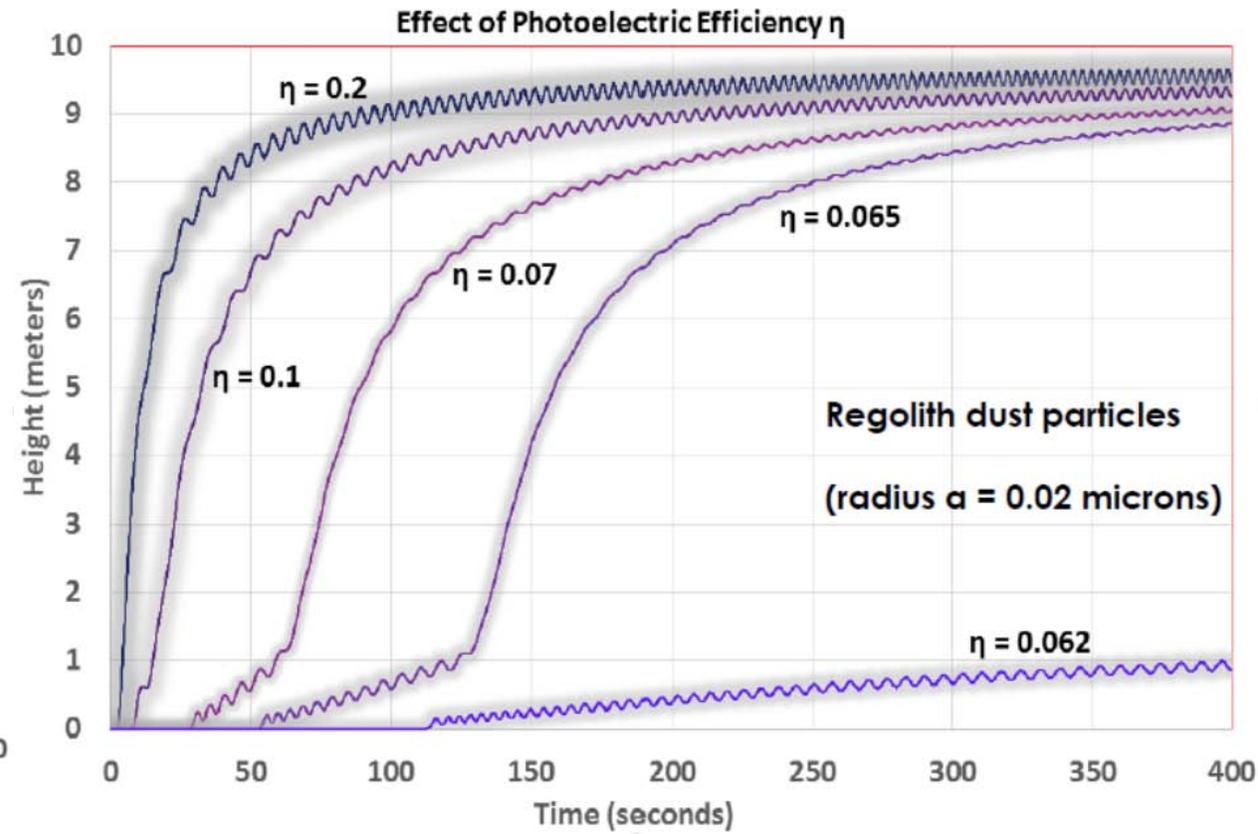
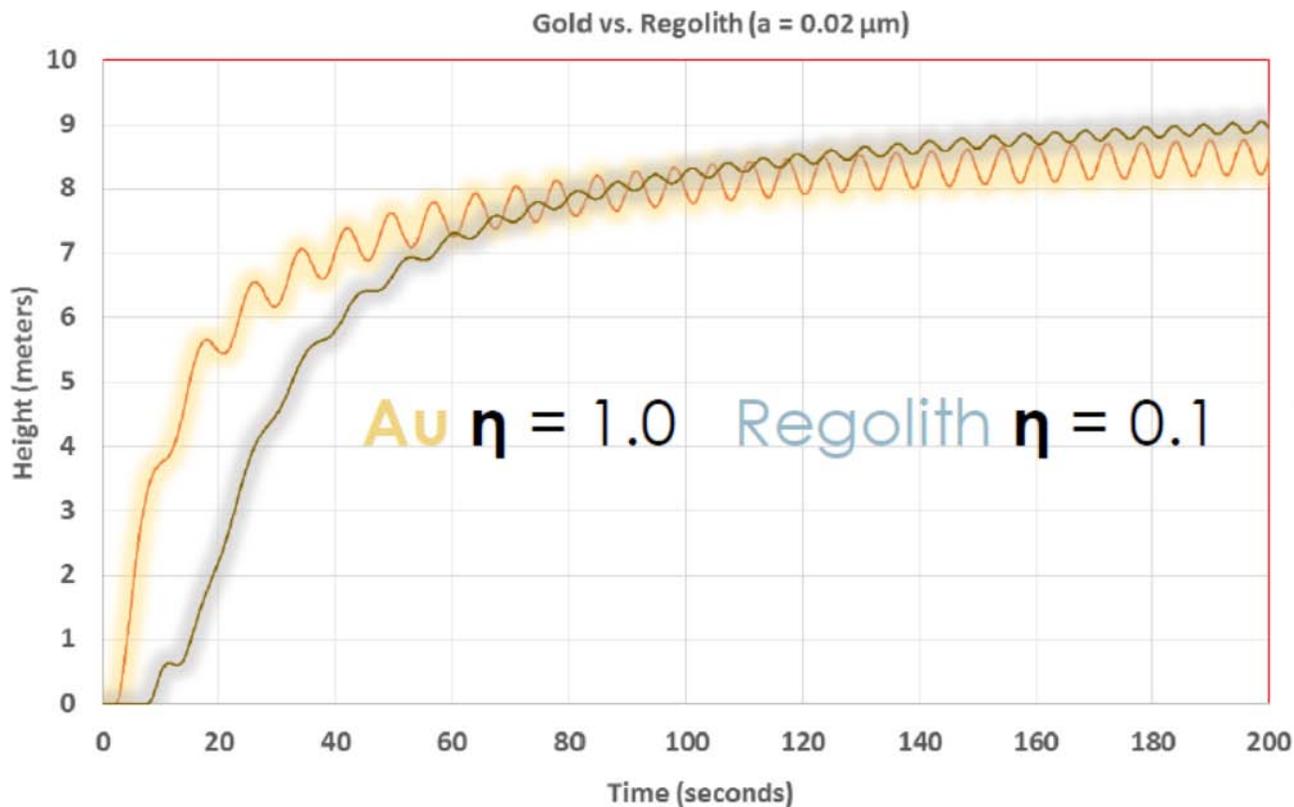


Electrostatic placer deposits of gold?

LCROSS implies ~0.5% Au (5,000 g/t)

Electrostatic forces favor gold dust transport

Will accumulate within anomalous craters

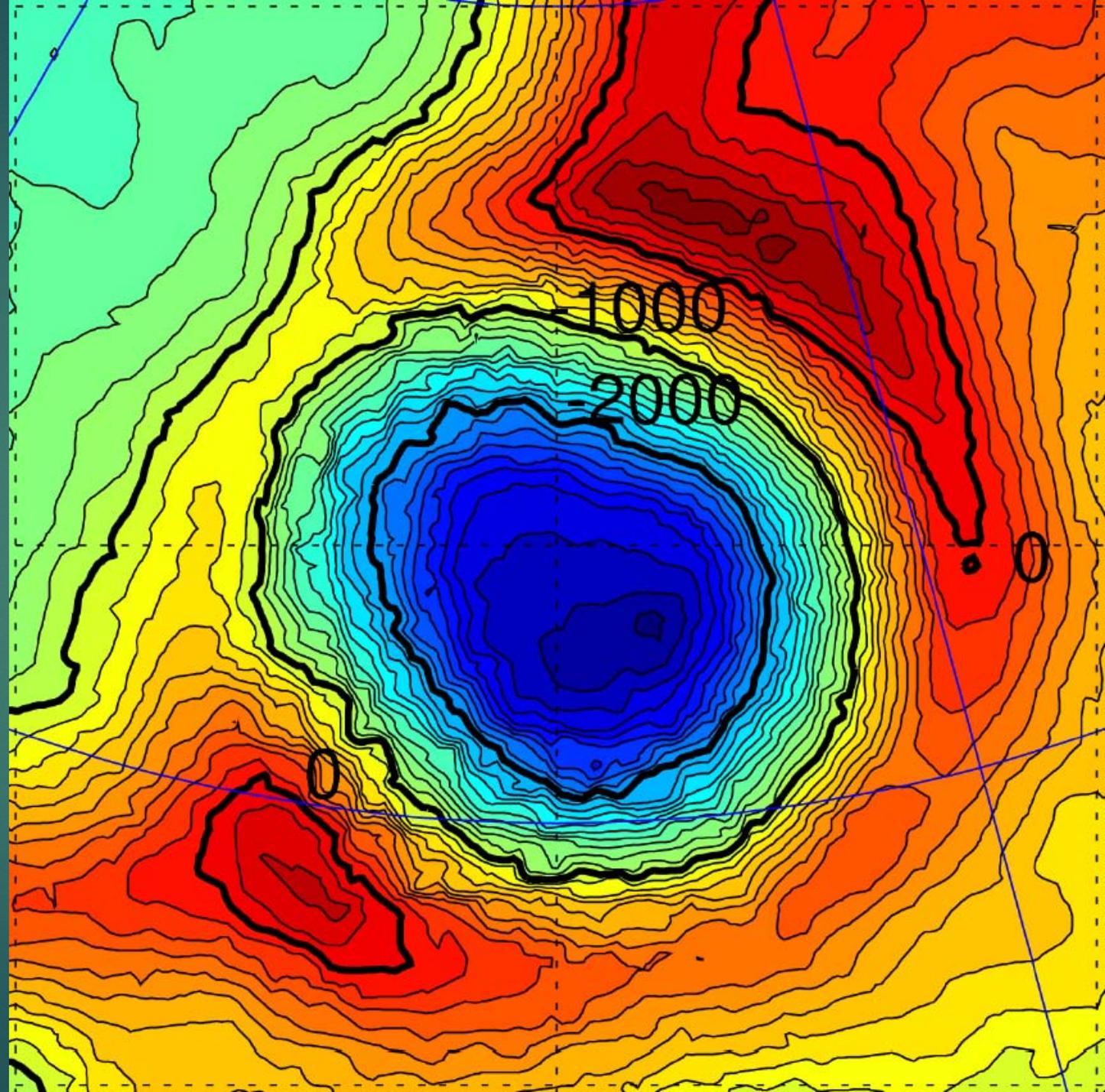


Whipple Crater

30° average slopes

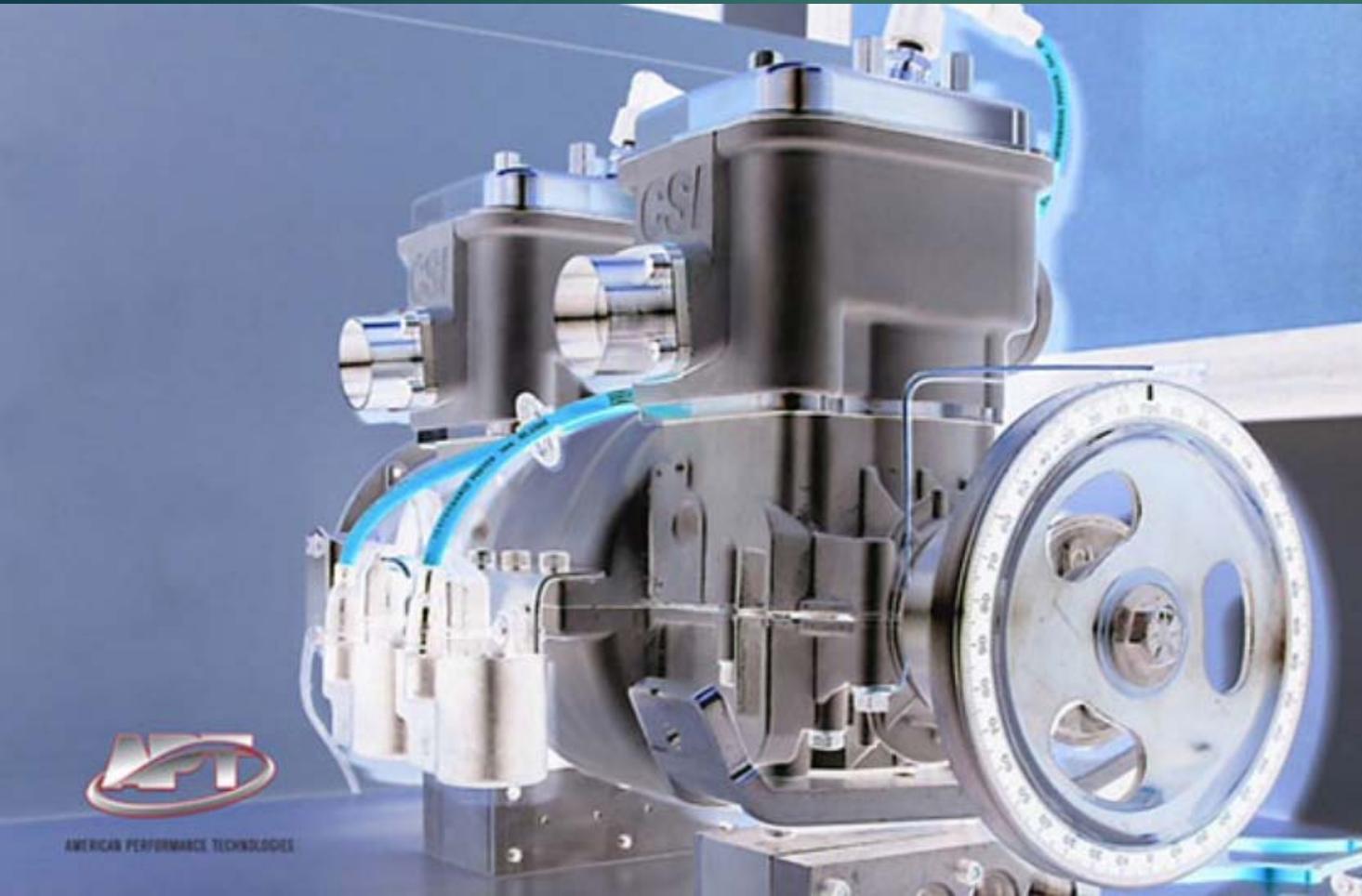
Impossible to
explore with RPM

Would have to land
in the middle



What we propose: ICESIP

An ICE-electric hybrid powered by the SonicFlow 2-cycle engine:



Burns no oil

High power density

40% TE

Fuel economy



AMERICAN PERFORMANCE TECHNOLOGIES

ICE-BOTE Trade Study

RPM-style rover:

100 kg total mass

30 kg propulsion mass budget

200 Watt average power

1000 Watt peak power



Battery Only Design

Tesla Roadster

30 Mass budget kg

5 Margin

25 Mass budget – Margin

25 Total Battery Mass

6.00×10^5 Specific Energy (J/kg)

1.50×10^7 Total Energy

0.9 Discharge efficiency

1.35×10^7 Net Energy available for system J

200 Average Power (W = J/s)

67,500 Time s

18.75 Time hr

0.78 Time day

Lithium Ion Battery

30 Mass budget kg

5 Margin

25 Mass budget - Margin

25 Total Battery Mass

2.00×10^6 Specific Energy (J/kg)

5.00×10^7 Total Energy

0.9 Discharge efficiency

4.50×10^7 Net Energy available for system J

200 Average Power (W = J/s)

225,000 Time s

62.50 Time hr

2.60 Time day

LH2/LO2 Design

ICE-hybrid vehicle LH2/LO2

30 Total Mass budget (kg)

5 Margin

25 Actual mass budget (kg)

0.186 Mass of ICE (kg)

0.223 Mass of generator/starter (kg)

0.409 Total mass ICE + generator kg

500 Battery specific power (W/kg)

1000 Peak Power (W)

2 Battery Mass (kg Li-S)

2.4 Total bat + ICE + generator (kg)

22.6 Mass budget for tankage & propellant

19.805 Mass of Propellant actually burned (kg)

17.604 Mass LO2

2.201 Mass of LH2

12.0% LH2 boiloff fudge factor

2.465 Total mass LH2

20.069 Total propellant mass (kg)

550.139 moles of O2

1100.278 moles of H2

0.5 molar O2/H2

1,141 Density of LO2 (kg/m³)

70.85 Density of LH2 (kg/m³)

0.01543 Volume of O2 (m³)

0.03479 Volume of H2 (m³)

50.2 Total Volume (L)

13.3 Total Volume (gal)

LH2/LO2 Design—Tankage

0.1544 Radius of O2 tank (m)

0.2025 Radius of H2 tank (m)

0.2997 Area of O2 tank (m²)

0.5153 Area of H2 tank (m²)

Liquid tank shell densities

0.9027 Inner tank: Al 2024-T81 (bi-grid) stiffened (kg/m²)

2.1919 Outer tank: DRA 55% (kg/m²)

3.09465 Total Tank unit weight (kg/m²)

0.93 mass LO2 tank (kg)

1.59 Mass LH2 tank (kg)

2.52 Total Tankage kg

22.59 Mass of tankage + propellant

22.6 Tankage & Fuel Mass budget

100.002% (Tankage + Propellant) / Mass budget

LH2/LO2 Design—Range Extension

285,800 H₂/O₂ molar Energy (J/mol H₂O)
1.59E+07 H₂/O₂ specific energy (J/kg)
3.14E+08 Total stored energy J
0.4 ICE thermal efficiency
1.26E+08 Rotary energy
0.9 Efficiency of generator
1.13E+08 Energy produced by generator J
0.9 Charge/discharge efficiency
1.02E+08 Energy released by batteries
200 average power
509,424 time s
141.5 time hr
5.90 time days

GH2/GO2 Design—Tankage

16.236 Mass of Propellant (kg)
14.432 Mass O2
1.804 Mass of H2
451.000 moles of O2
902.000 moles of H2
0.5 O2/H2
10,152 Pressure psi
70,000,000 Pressure Pa
0.0157028 Volume of O2 (m³)
0.0314057 Volume of H2 (m³)
47.1 Total Volume (L)
12.4 Total Volume (gal)

0.1553 Radius of O2 tank (m)
0.1957 Radius of H2 tank (m)
0.3033 Area of O2 tank (m²)
0.4814 Area of H2 tank (m²)
2,700 Density of Al (kg/m³)
3.00E-03 Thickness of tanks (m)
9.10E-04 Volume of O2 tank shell (m³)
1.44E-03 Volume of H2 tank shell (m³)
2.46 mass of O2 tank
3.90 Mass of H2 tank
6.36 Total Tankage kg
16.24 Mass of Propellant (kg)
22.59 Mass of tankage + propellant
22.6 Mass budget
100.002% Budget – (tankage + Prop)

GH2/GO2 Design—Range Extension

285,800 H₂/O₂ molar Energy (J/kg)
1.59E+07 H₂/O₂ specific energy (J/kg)
2.58E+08 Total stored energy J
0.4 ICE thermal efficiency
1.03E+08 Total work done by ICE
0.9 Efficiency of generator
9.28E+07 Energy produced by generator J
0.9 Charge/discharge efficiency
8.35E+07 Energy released by batteries
200 average power
417,622 time s
116.0 time hr
4.83 time days

LCH₄/LO₂
comparable
to GH₂/GO₂

Other Considerations

- “Waste heat” = useful enthalpy
- 300 Watts available for heating LPER
- Can also be used for instruments like OVEN
- Battery-only designs must produce heat from electricity

- Flex fuel capability

- Residual propellants from the lander can further extend mission time

